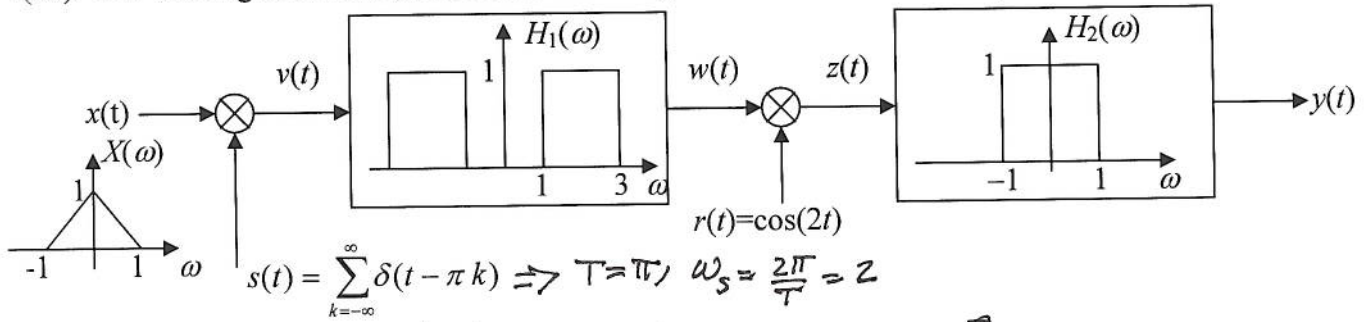
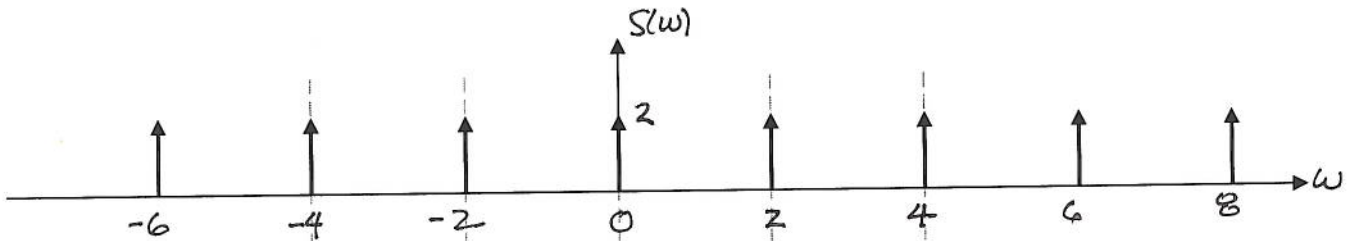


### Assignment #13 - Solutions

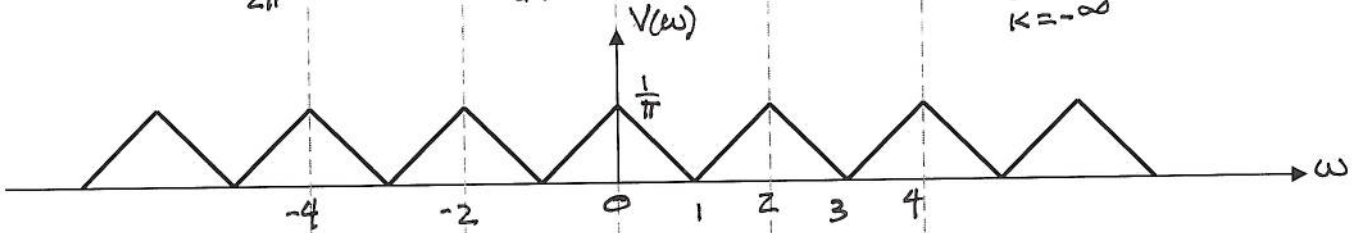
1(35). For the diagram shown, sketch the following waveforms. Label all key values.



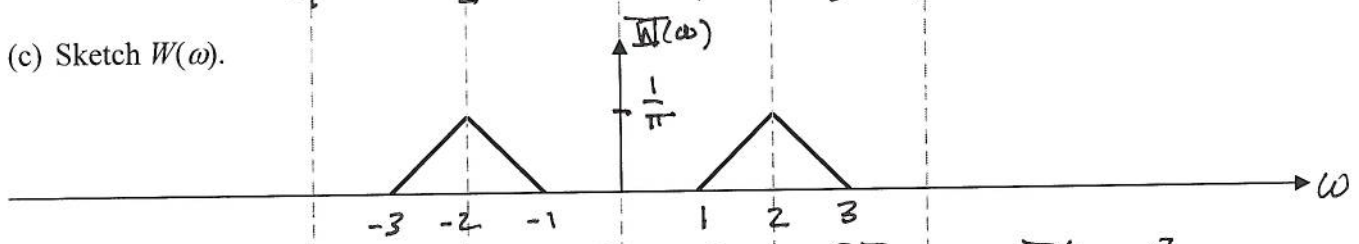
(a) Sketch  $S(\omega)$ . 
$$s(t) = \sum_{k=-\infty}^{\infty} \frac{1}{\pi} e^{jk\omega t} \leftrightarrow S(\omega) = \sum_{k=-\infty}^{\infty} \frac{1}{\pi} 2\pi S(\omega - k\omega_s) = \sum_{k=-\infty}^{\infty} 2 S(\omega - 2k)$$



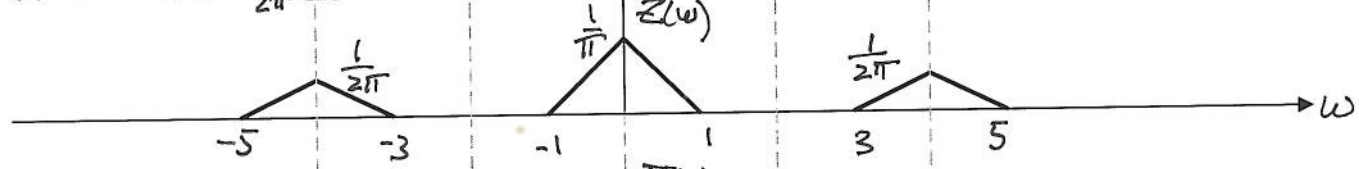
(b) Sketch  $V(\omega) = \frac{1}{2\pi} X(\omega) * S(\omega) = \frac{1}{2\pi} X(\omega) * \sum_{k=-\infty}^{\infty} 2 S(\omega - 2k) = \frac{1}{\pi} \sum_{k=-\infty}^{\infty} X(\omega - 2k)$



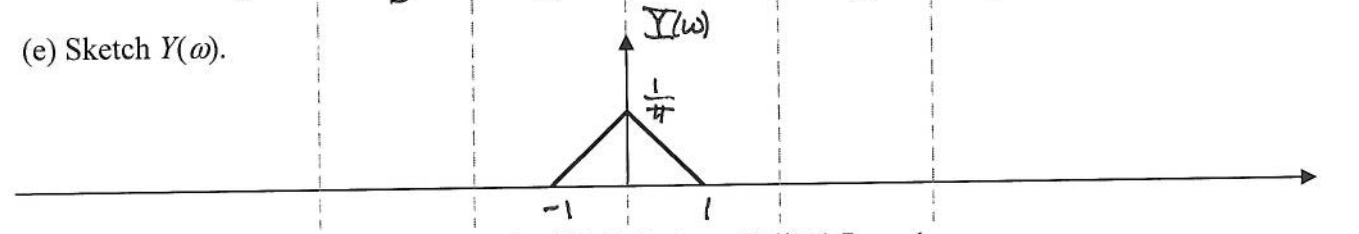
(c) Sketch  $W(\omega)$ .



(d) Sketch  $Z(\omega) = \frac{1}{2\pi} W(\omega) * \pi [S(\omega - 2) + S(\omega + 2)] = \frac{1}{2} [W(\omega - 2) + W(\omega + 2)]$

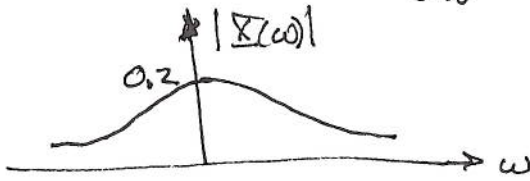


(e) Sketch  $Y(\omega)$ .



2(20). Are the following signals bandlimited? Explain why or why not.

(a)  $x(t) = e^{-5t}u(t) \leftrightarrow \bar{X}(\omega) = \frac{1}{5 + j\omega}$



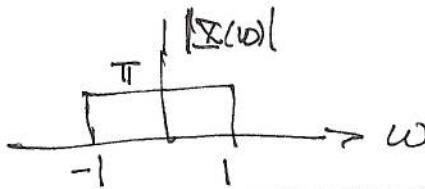
Not bandlimited

(b)  $x(t) = \text{sinc}(t)$

Using  $\frac{\omega}{\pi} \text{sinc}(\omega t) \leftrightarrow$

$W = 1$

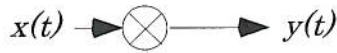
$\text{sinc}(t) \leftrightarrow$



yes, Band limited with  $\omega_{max} = 1$

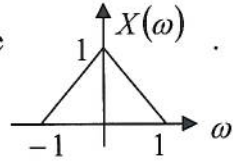
3(20). Two signals are multiplied as shown, where  $c(t)$  is the impulse train,  $c(t) = \sum_{k=-\infty}^{\infty} \delta(t - kT)$ , with

$$T = \frac{2\pi}{3} \text{ sec.}$$



$$c(t) = \sum_{k=-\infty}^{\infty} \delta(t - kT) \leftrightarrow C(\omega) = \frac{2\pi}{T} \sum_{k=-\infty}^{\infty} \delta(\omega - k\omega_s), \quad \omega_s = \frac{2\pi}{T} = \frac{2\pi}{2\pi/3} = 3$$

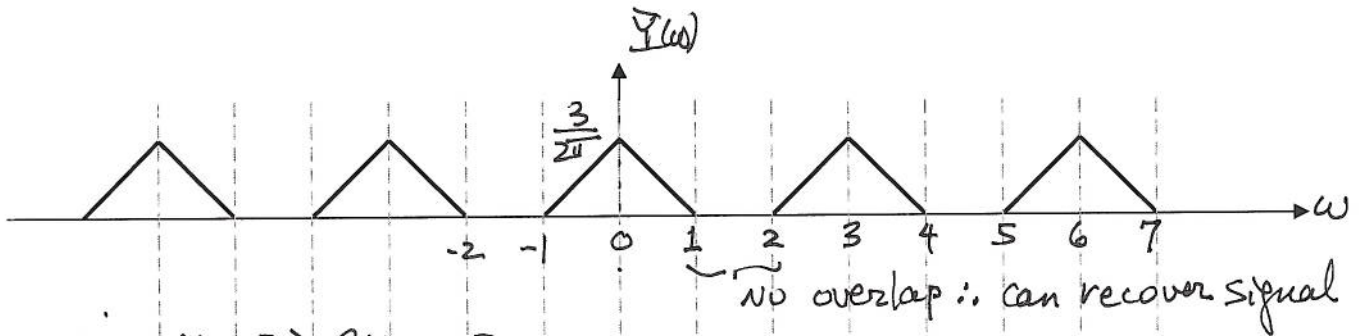
(a) Let the spectrum of  $x(t)$  be  $X(\omega)$ . Sketch the spectrum of  $y(t)$ ,  $Y(\omega)$ . Can  $x(t)$  be



recovered from  $y(t)$  using lowpass filtering? Why or why not?

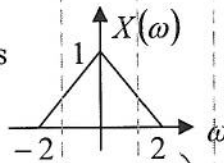
$$y(t) = x(t)c(t) \leftrightarrow Y(\omega) = \frac{1}{2\pi} X(\omega) * C(\omega) = \frac{1}{2\pi} X(\omega) * \sum_{k=-\infty}^{\infty} \frac{2\pi}{T} \delta(\omega - k\omega_s) = \frac{1}{T} \sum_{k=-\infty}^{\infty} X(\omega - k\omega_s)$$

$$\text{For } T = \frac{2\pi}{3}, \omega_s = 3 \quad Y(\omega) = \frac{3}{2\pi} \sum_{k=-\infty}^{\infty} X(\omega - k3)$$

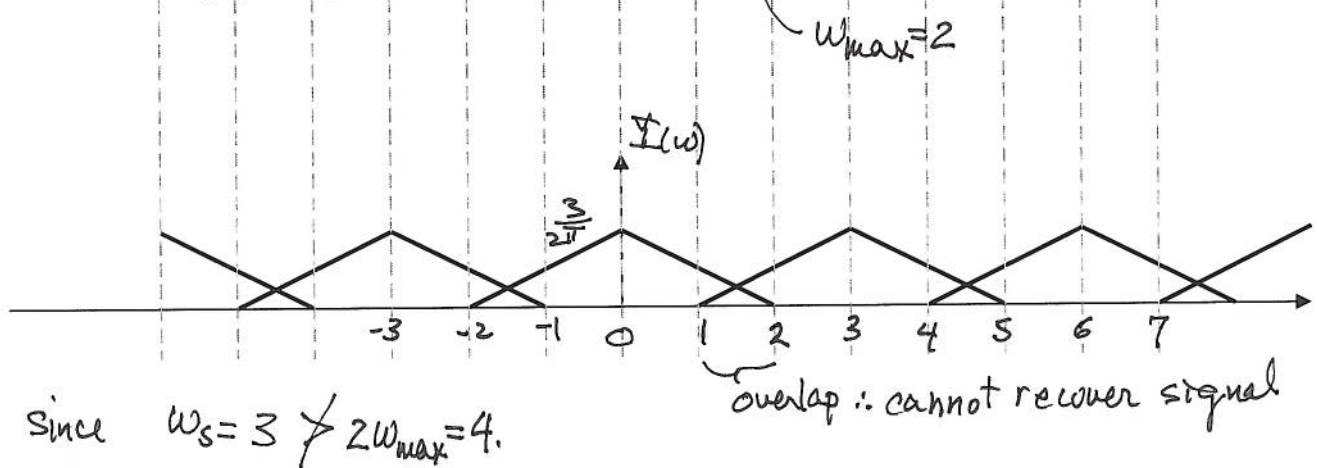


$$\text{Since } \omega_s = 3 > 2\omega_{\max} = 2$$

(b) Repeat part (a) if the spectrum of  $x(t)$  is  $X(\omega)$  and  $c(t)$  remains the same. Can  $x(t)$  be

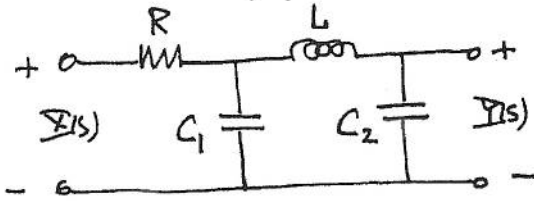


recovered from  $y(t)$  using lowpass filtering? Why or why not?



$$\text{Since } \omega_s = 3 < 2\omega_{\max} = 4.$$

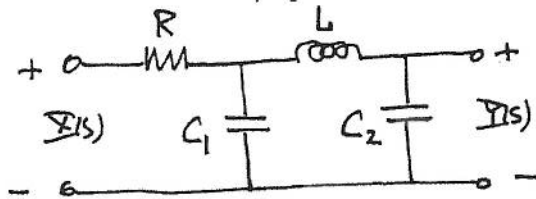
4(25). Find the transfer function  $H(s) = \frac{Y(s)}{X(s)}$ , where  $C_1 = \frac{1}{6}$ ,  $C_2 = \frac{1}{2}$ ,  $L = 4$ ,  $R = 3$ .



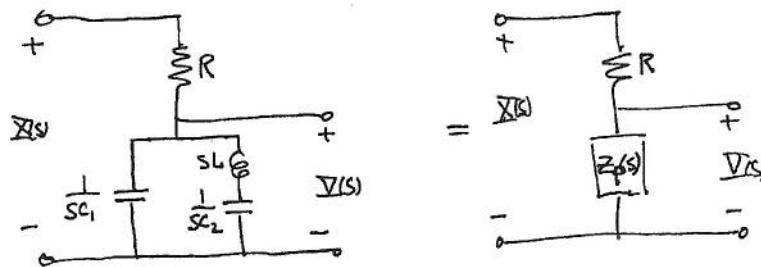
From: **Note #43. Butterworth Filters**

### 3. Realization of Filter as RCL Circuit.

Verify that the third order Butterworth filter transfer function,  $B(s) = \frac{\omega_c^3}{s^3 + 2\omega_c s^2 + 2\omega_c^2 s + \omega_c^3}$ , is realized by the circuit. Express the elements  $C_1, C_2, L$  in terms of  $R$  and the cutoff frequency,  $\omega_c$ .



Method 1. First find the circuit transfer function using the voltage divider law. This is done in two steps. First find  $V(s)$  and then  $Y(s)$ .



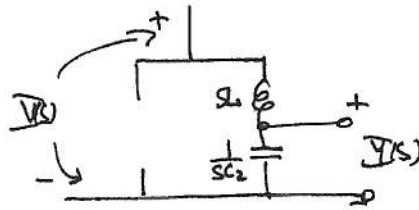
Therefore,

$$\frac{V(s)}{X(s)} = \frac{Z_p(s)}{R + Z_p(s)}, \text{ where } Z_p(s) = \frac{\left(\frac{1}{sC_1}\right)\left(\frac{1}{sC_2} + sL\right)}{\frac{1}{sC_1} + \frac{1}{sC_2} + sL} = \frac{1 + s^2LC_2}{s(C_1 + C_2) + s^3LC_1C_2},$$

and

$$\frac{Y(s)}{X(s)} = \frac{1 + s^2LC_2}{sR(C_1 + C_2) + Rs^3LC_1C_2 + 1 + s^2LC_2}.$$

Expressing  $Y(s)$  in terms of  $V(s)$



results in

$$\frac{Y(s)}{V(s)} = \frac{\frac{1}{sC_2}}{sL + \frac{1}{sC_2}} = \frac{1}{1 + s^2 LC_2}$$

Combining the two transfer functions,

$$\begin{aligned} \frac{Y(s)}{X(s)} &= \frac{V(s)}{X(s)} \cdot \frac{Y(s)}{V(s)} = \frac{1 + s^2 LC_2}{sR(C_1 + C_2) + Rs^3 LC_1 C_2 + 1 + s^2 LC_2} \cdot \frac{1}{1 + s^2 LC_2} \\ &= \frac{1}{RLC_1 C_2} \\ &= \frac{1}{s^3 + s^2 \left( \frac{1}{RC_1} \right) + s \left( \frac{C_1 + C_2}{LC_1 C_2} \right) + \frac{1}{RLC_1 C_2}} \end{aligned}$$

Comparing this equation term by term to

$$B(s) = \frac{\omega_c^3}{s^3 + 2\omega_c s^2 + 2\omega_c^2 s + \omega_c^3}$$

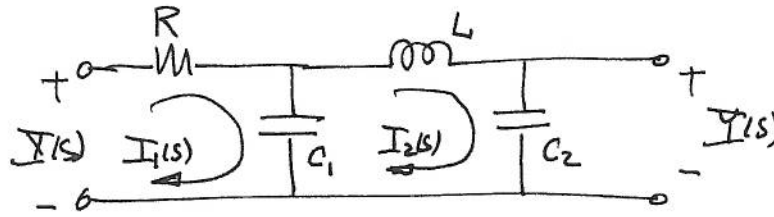
yields

$$\frac{1}{RLC_1 C_2} = \omega_c^3, \quad \frac{1}{RC_1} = 2\omega_c, \quad \frac{C_1 + C_2}{LC_1 C_2} = 2\omega_c^2$$

Solving simultaneously for  $L, C_1, C_2$ , gives us

$$C_1 = \frac{1}{2R\omega_c}, \quad C_2 = \frac{3}{2R\omega_c}, \quad L = \frac{4R}{3\omega_c}$$

Method #2. Using Kirchoff's voltage law



results in the equations

$$\left(R + \frac{1}{sC_1}\right)I_1(s) - \frac{1}{sC_1}I_2(s) = X(s)$$

$$-\frac{1}{sC_1}I_1(s) + \left(\frac{1}{sC_1} + sL + \frac{1}{sC_2}\right)I_2(s) = 0$$

Simplifying,

$$(RsC_1 + 1)I_1(s) - I_2(s) = sC_1X(s)$$

$$-sC_2I_1(s) + (s^3LC_1C_2 + s(C_1 + C_2))I_2(s) = 0$$

Now solve for  $I_2(s)$  using Cramer's rule,

$$I_2(s) = \frac{\begin{vmatrix} RsC_1 + 1 & sC_1X(s) \\ -sC_2 & 0 \end{vmatrix}}{\begin{vmatrix} RsC_1 + 1 & -1 \\ -sC_2 & s^3LC_1C_2 + s(C_1 + C_2) \end{vmatrix}},$$

or

$$I_2(s) = \frac{sC_2X(s)}{s^3LRC_1C_2 + s^2LC_2 + sR(C_1 + C_2) + 1}$$

Then the output is

$$Y(s) = \frac{1}{sC_2}I_2(s) = \frac{X(s)}{s^3LRC_1C_2 + s^2LC_2 + sR(C_1 + C_2) + 1}$$

resulting in the transfer function,

$$H(s) = \frac{Y(s)}{X(s)} = \frac{1}{s^3LRC_1C_2 + s^2LC_2 + sR(C_1 + C_2) + 1}$$

or in standard form,

$$H(s) = \frac{1}{LRC_1C_2} \cdot \frac{1}{s^3 + s^2 \left( \frac{1}{RC_1} \right) + s \left( \frac{C_1 + C_2}{LC_1C_2} \right) + \frac{1}{LRC_1C_2}}$$

For  $C_1 = \frac{1}{6}$ ,  $C_2 = \frac{1}{2}$ ,  $L = 4$ ,  $R = 3$

$$\frac{1}{LRC_1C_2} = \frac{1}{4(3)\left(\frac{1}{6}\right)\left(\frac{1}{2}\right)} = 1$$

$$\frac{1}{RC_1} = \frac{1}{3\left(\frac{1}{6}\right)} = 2$$

$$\frac{C_1 + C_2}{LC_1C_2} = \frac{\frac{1}{6} + \frac{1}{2}}{4\left(\frac{1}{6}\right)\left(\frac{1}{2}\right)} = \frac{\frac{2}{3}}{\frac{2}{3}} = 2$$

$$\therefore H(s) = \frac{1}{s^3 + 2s^2 + 2s + 1}$$

A third order Butterworth filter.